

MODELLING AND SIMULATION OF A RECTANGULAR MICROSTRIP ANTENNA IN MATLAB WORKING ENVIRONMENT

Abdul Rasak Zubair & Sheriff Olayemi
Department of Electrical/Electronic Engineering
Email: ar.zubair@yahoo.co.uk

ABSTRACT

Modelling and simulation of a rectangular microstrip patch antenna on MATLAB platform is presented in form of three algorithms. The design algorithm which computer the dimensions of the rectangular microstrip patch antenna is based on the transmission line model. The cavity model algorithm analysis the rectangular microstrip patch antenna. The radiation pattern algorithm plots the radiation patterns of the antenna. The algorithms developed were used to model and simulate three different specifications of rectangular patch antenna. The results obtained are found to compare favourably with existing records.

Keywords: Antenna, Microstrippatch, Transmission line model, Cavity model, Radiation pattern

INTRODUCTION

Microstrip antenna technology began its rapid development in the late 1970s. By the early 1980s, primary microstrip antenna elements and arrays were relatively well established in terms of design and modeling [1]. Microstrip antennas have received a lot of attention because of their many advantages. These advantages include low profile, low cost, conformability to planar and non-planar surfaces and ease of integration with active devices [2]. The microstrip patch

antenna consists of three basic parts; the radiating patch, the dielectric substrate and the ground plane as illustrated in Fig. 1. The dielectric substrate is located between the radiating patch and the ground plane. The radiating patch is made of any conducting material and it can take up any shape depending on the design requirements. Some of the most common shapes of radiating patch are shown in Fig 2. The ground plane is a metal plate bonded to one side of the dielectric substrate.

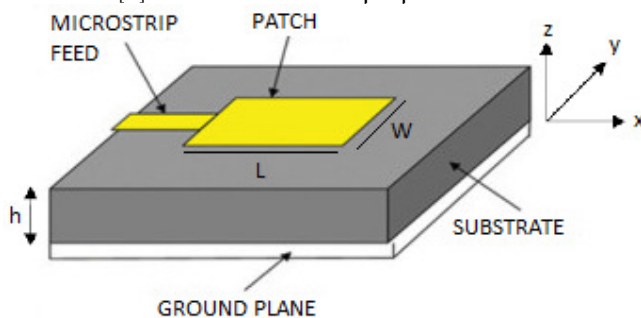


Fig. 1 Microstrip patch antenna

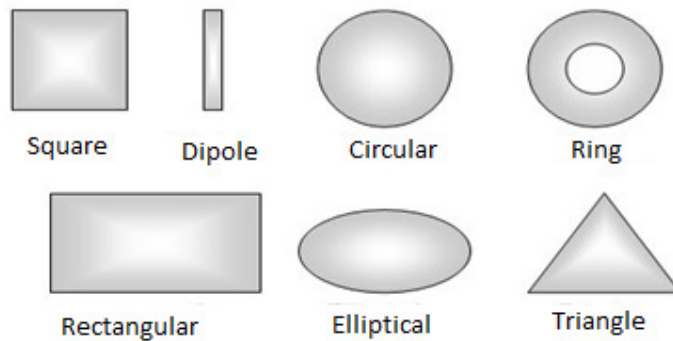


Fig. 2: Common shapes for radiating patch.

It is necessary to predict exactly how an antenna will behave prior to actual fabrication. Modelling and simulation predict the radiation characteristics of an antenna and suggest necessary modifications before fabrication. There are currently several full electromagnetic modelling tools and products such as Ansoft Ensemble, High Frequency Structure Simulation (HFSS) and Computer Simulation Technology and Microwave Studio (CST MS) that are used in the modelling and simulation of complex circuits and antennas [3]. However, a lot of these software's come at a very steep price and are sometimes proprietary [4]. It is possible to implement the modelling and simulation entirely on MATLAB platform and this makes it much more accessible and affordable to students and designers. MATLAB is a ubiquitous math, data manipulation, signal processing, and graphics software package [5]. It can be used effectively in the design and analysis of antenna. In this work, modelling and

simulation of a rectangular microstrip antenna are implemented in MATLAB working environment.

MICROSTRIP PATCH ANTENNAS

Microstrippatch antennas are analysed using any of the three following models; the transmission line model, the cavity model and the full wave model [6]. The transmission line model is the easiest to implement and it gives adequate insight into the physical attributes of the antenna [7]. The cavity model is much more accurate and much more complex than the transmission line model. The full wave model is the most accurate and most complex of the three models as it can be used to analyse all shapes and all arrangements of patch element [8]. The transmission line model is selected in this work to calculate the physical dimensions of the antenna. The cavity model is used to analyse and plot the radiation patterns of the antenna. Fig. 3 illustrate the sequence of steps involved in the modelling

and simulation of microstrip patch antenna.

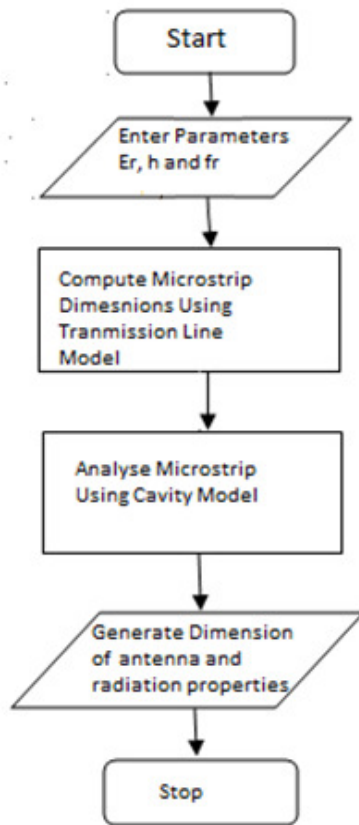


Fig. 3 Sequence of steps involved in the modelling and simulation of the microstrippatch antenna

Transmission Line Model

The top view of a typical rectangular microstrip antenna patch is shown in Fig 4. W is the width of the patch, L is the actual length of the patch, w_0 is the width of the feed and ϵ_r is the dielectric constant of the substrate. h is the distance between the patch and the ground plane which may represent the thickness of the substrate. The fringing effect comes into play as the dimensions of the radiating patch are finite and the fields at the edge undergo fringing [9]. Fringing makes the microstrip

look wider electrically compared to its physical dimensions and since some of the waves travel in the substrate and some in air, an effective dielectric constant ϵ_{eff} is introduced to account for this fringing effect and the wave propagation in the line. This would make the microstrip patch appear as shown in Fig. 5. The transmission line equations that govern the transmission line model are given by Eqns. (1), (2), (3), (4) and (5) [6].

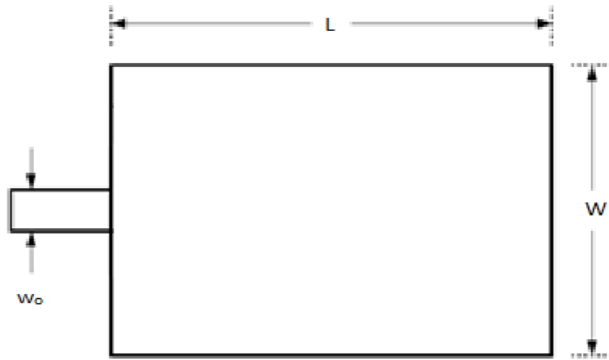


Fig 4. Typical Microstrip Antenna Patch.

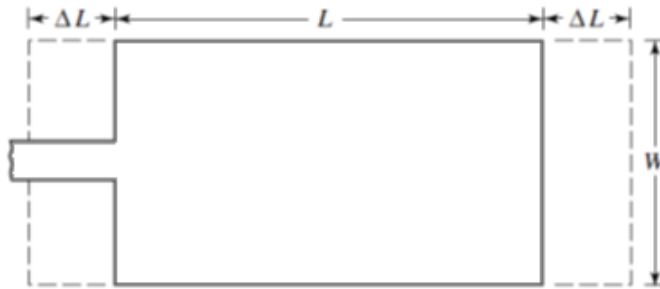


Fig. 5 Top view of the patch antenna showing effect of fringing on effective length L_{eff} .

$$W = \frac{v_0}{2f_r} \sqrt{\frac{2}{\epsilon_r + 1}} \quad (1)$$

where v_0 is the speed of light in free space and f_r is the resonant frequency.

$$\epsilon_{r_{eff}} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r + 1}{2} \left(1 + 12 \frac{h}{W}\right)^{-1/2} \quad (2)$$

$$\Delta L = 0.412h \frac{(\epsilon_{r_{eff}} + 0.3) \left(\frac{W}{h} + 0.264\right)}{(\epsilon_{r_{eff}} - 0.258) \left(\frac{W}{h} + 0.8\right)} \quad (3)$$

$$L = \frac{v_0}{2f_r \sqrt{\epsilon_{r_{eff}}}} - 2\Delta L \quad (4)$$

Where L is the actual length of the microstrip.

$$L_{eff} = L + 2\Delta L \quad (5)$$

Furthermore, the transmission line model estimates the impedance of the microstrip at the feed point. The two widths of the patch are treated as slots and each radiating slot is represented by a parallel equivalent admittance Y (with conductance G and susceptance B) as illustrated in Fig. 6 [10]. The two radiating slots are similar and have equal conductance (G) and equal susceptance (B) as described in Eqn. (6). G and B are as given by Eqns. (7) and (8) respectively [6]. The mutual conductance G_{12} and input resistance R_{in} are given by Eqns. (9) and (10) [6].

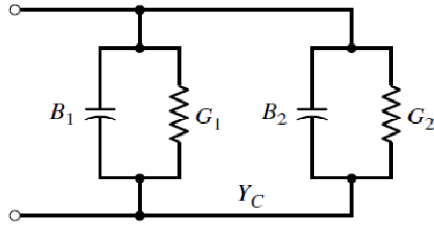


Fig 6. Transmission line equivalent circuit

$$G_2 = G_1 = G; B_2 = B_1 = B \quad (6)$$

$$G = \frac{W}{120\lambda_0} \left(1 - \frac{1}{24}(k_0h)^2\right) \quad \text{for } \frac{h}{\lambda_0} < \frac{1}{10} \quad (7)$$

where λ_0 is free space wavelength.

$$B = \frac{W}{120\lambda_0} \left(1 - 0.636 \ln(k_0h)\right) \quad \text{for } \frac{h}{\lambda_0} < \frac{1}{10} \quad (8)$$

$$G_{12} = \frac{1}{120\pi^2} \int_0^\pi \left(\frac{\sin\left(\frac{k_0W}{2}\cos(\theta)\right)}{\cos(\theta)}\right)^2 J_0(k_0L\sin(\theta)) \sin^3(\theta) d\theta \quad (9)$$

where J_0 is a Bessel function of the first kind of order zero. θ is one of the angles that describes the H plane and E plane.

$$R_{in} = \frac{1}{2(G_1 \pm G_{12})} \quad (10)$$

Another way to change the resonant input resistance is by an inset feed recessed a distance y_0 and is shown in Fig 7. Varying input resistance is just to achieve matching.

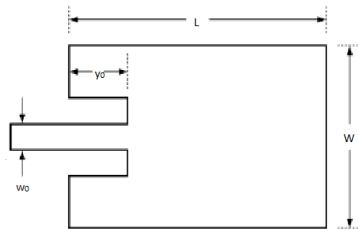


Fig 7. Inset feed on microstrip patch

Finding the inset feed distance y_0 entails knowing the characteristic impedance of the microstrip line feed. Its impedance Z_c is a function of w_0 , h and ϵ_{reff} [6]. w_0 is subject to the condition in Eqn. (11). Equations (12) and (13) give Z_c [6]. Eqn. (14) gives the admittance while Eqn. (15) calculates the input resistance. Finding the inset distance involves solving an

optimization problem that minimizes the objective function of Eqn. (16). Based on these mathematical equations, a computer program was developed to be used in the first phase of the microstrip antenna modelling and the flow chart is shown in Fig 8.

$$w_0 \ll W \quad (11)$$

$$Z_c = \frac{60}{\sqrt{\epsilon_{reff}}} \ln \left[\frac{8h}{W_0} + \frac{W_0}{4h} \right] \quad \text{If } \frac{W_0}{h} \leq 1 \quad (I2)$$

$$Z_c = \sqrt{\epsilon_{reff}} \left[\frac{W_0}{h} + 1.393 + 0.667 \ln \left(\frac{W_0}{h} + 1.444 \right) \right] \quad \text{If } W_0 > 1 \quad (I3)$$

$$Y_c = \frac{1}{Z_c} \quad (I4)$$

$$R_{in}(y = y_0) = \frac{1}{2(G_1 \pm G_{12})} \left(\cos^2 \left(\frac{\pi}{L} y_0 \right) + \frac{G_1^2 + B_1^2}{Y_c^2} \sin^2 \left(\frac{\pi}{L} y_0 \right) - \frac{B_1}{Y_c} \sin \left(\frac{2\pi}{L} y_0 \right) \right)$$

$$(I5)$$

$$\min_{y_0} Z_0 - R_{in} \text{ such that } 0 \leq y_0 \leq L/2 \quad (I6)$$

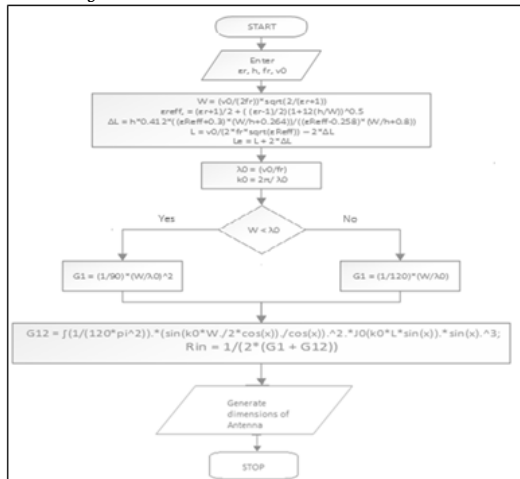


Fig. 8 Flow Chart showing implementation of transmission line model

Cavity Model

Microstrip antennas resemble dielectric-loaded cavities, and they exhibit higher order resonances [11]. The normalized fields within the dielectric substrate (between the patch and the ground plane) can be found more accurately by treating that region as a cavity bounded by electric conductors (above and below it) and by magnetic walls (to simulate an open circuit) along the perimeter of the patch [12]. This is an approximate model which in principle leads to a reactive input impedance (of zero or infinite value of resonance) and it does not radiate any power. Although, the actual

fields are approximate to those generated by such a model, the computed pattern, input admittance, and resonant frequencies compare well with measurements. This model is suitable for finding the radiation pattern of the microstrip antenna. In the TM_{010} mode, the total field is the sum of the fields due to two elements array (each representing a slot) [13]. Since the slots are identical, this can be accomplished using an array factor for the two slots. In spherical coordinates, the far-zone electric field is given by Eqn. (17). Using the array factor (AF) of Eqn. (18) gives the total radiated field of Eqn. (19).

Modelling and Simulation of a Rectangular Microstrip Antenna in Matlab Working Environment

$$E_r \approx 0; E_\theta \approx 0; E_\phi = j \frac{k_0 h W E_0 e^{-jk_0 r}}{2\pi r} \left\{ \sin\theta \frac{\sin(X)}{X} \frac{\sin(Z)}{Z} \right\} \quad (17)$$

where $X = \frac{k_0 h}{2} \sin\theta \cos\phi$ and

$$Z = \frac{k_0 W}{2} \cos\theta$$

$$(AF)_y = 2 \cos\left(\frac{k_0 L_e}{2}\right) \sin\theta \sin\phi$$

(18)

where L_e is the separation distance in the y direction and the effective length.

$$E_\phi^t =$$

$$j \frac{k_0 h W E_0 e^{-jk_0 r}}{2\pi r} \left\{ \sin\theta \frac{\sin(X)}{X} \frac{\sin(Z)}{Z} \right\} 2 \cos\left(\frac{k_0 L_e}{2}\right) \sin\theta \sin\phi \quad (19)$$

Therefore the E-plane field is obtainable by substituting $\theta = 90^\circ, 0^\circ \leq \phi \leq 90^\circ, 270^\circ \leq \phi \leq 360^\circ$ in Eqn. (19). The H-plane field is obtainable by substituting

$\phi = 0^\circ, 0 \leq \theta \leq 180$ in Eqn. (19).

Eqns (20), (21) and (22) define important metrics of microstrip antenna. The flow chart detailing the cavity model analysis is shown in Fig 9. Fig. 10 shows the flow chart of a separate algorithm which is developed to plot of the radiation properties such as the electric field plot and magnetic field plot.

Return loss, RL (dB) =

$$10 \log_{10} P_i / P_r \quad (20)$$

Where P_i = incident power and P_r = reflected power

Reflection coefficient, $RC =$

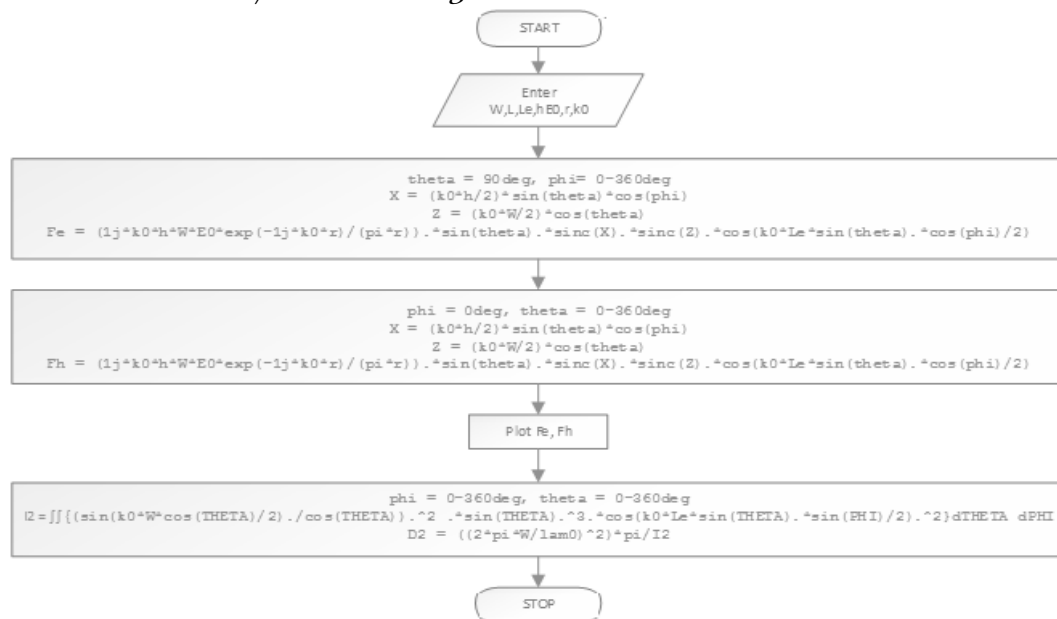
$$\frac{Z_l - Z_s}{Z_l + Z_s} \quad (21)$$

Where Z_l = load impedance and

Z_s = source impedance

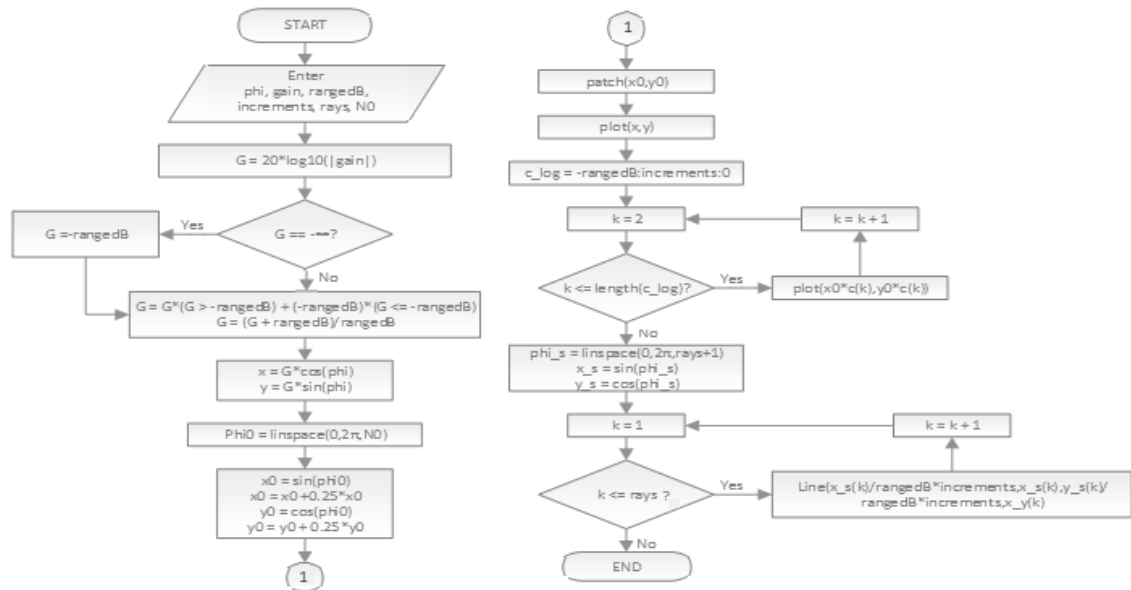
Voltage Standing Wave Ratio, $VSWR =$

$$\frac{1+RC}{1-RC} \quad (22)$$



where $\theta = \theta, \phi = \pi$

Fig 9. Flow chart showing the cavity model



where $\theta = \theta$, $\pi = \pi$

Fig 10 Flow chart showing the code for radiation pattern plotting

RESULTS

Transmission Line Model Results

Three separate microstrip antennas, Antenna A, B and C were modelled and simulated with the developed algorithms. Antenna A was designed to operate at a frequency of 10GHz and it has a substrate dielectric constant of 2.2 with a

chosen height of 0.1588cm. Antenna B was designed to operate at a frequency of 2.4GHz with dielectric constant of 3.4 and a height of 0.1500cm. Antenna C was designed to operate at a frequency of 2.25GHz with a dielectric constant of 4.4 and a height of 0.1600cm.

Table I. Microstrip Design Parameters for Antenna A, B and C

	Description	Antenna A	Antenna B	Antenna C
Design Specifications	Frequency	10.00 GHz	2.40 GHz	2.25 GHz
	Substrate Permittivity, ϵ	2.2	3.4	4.4
	Height, h	0.1588	0.1500 cm	0.1600 cm
Patch's Dimensions and Parameters	Length of Patch, L	0.9061 cm	3.3471cm	3.1443cm
	Effective Length of Patch, L_e	1.0683cm	3.4914cm	3.2922cm
	Width of Patch, W	1.1859cm	4.2137cm	4.0572cm
	Substrate Effective Permittivity, ϵ_{eff}	1.9716	3.2045	4.1006
	Transmission Line Width, w_0	0.0237cm	0.0843cm	0.0811cm
	Insertion Point at $Z_c = 50 \Omega$, y_0	0.2962cm	1.1807cm	1.1555cm

Variation of Input impedance with Inset distance

The input impedance for varying inset distances $0 \leq y_0 \leq L/2$ for the inset feed for the three antennas A, B and C are shown in the figure 11 (a), (b) and (c) respectively. It can

be seen that the input impedance continues to decrease until it gets to a desired minimum for all the three antennas. This minimum inset distance is selected as the insertion point, y_0 for each Antenna as recorded in Table 1.

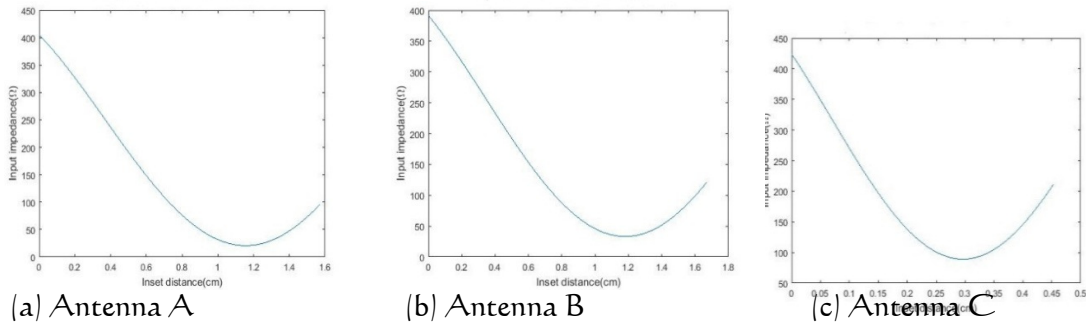


Fig 11 Variation of input impedance with inset distance

Radiation Pattern

The electric field plot and the magnetic field plot are both derived for antennas A, B and C. These are presented in Figures 12 and 13. Table 4 shows the values of reflection

coefficient (RC), return loss (RL) and VSWR at different insertion points (y_0). The directivity of Antennas A, B and C are obtained as 5.4376 dB, 4.3944 dB and 4.0551 dB respectively.

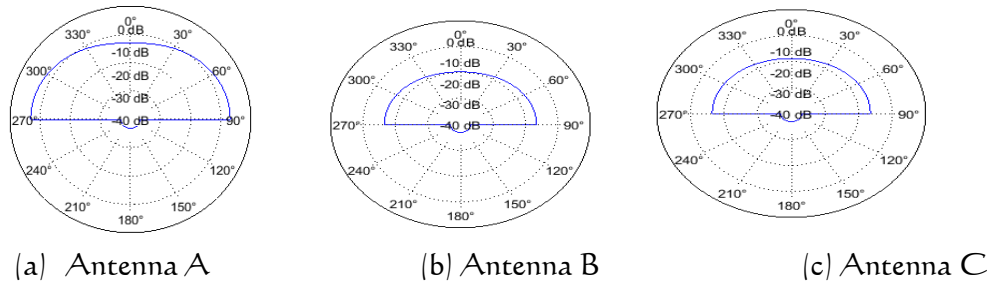


Fig 12. E-Field plot of Antenna A, B and C modelled.

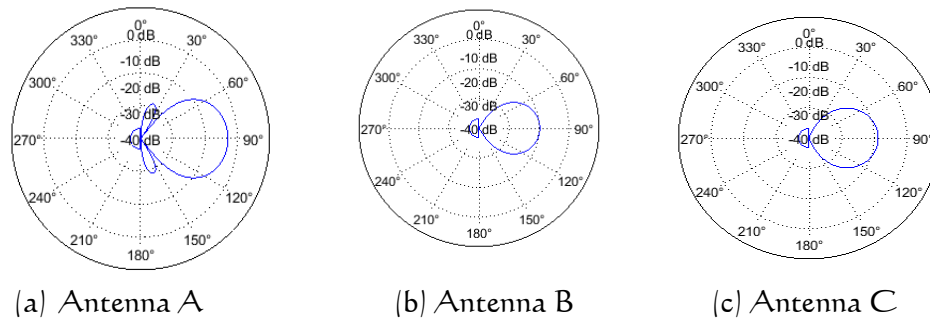


Fig 13 H-Field plot of Antenna A, B and C modelled

Table 4 Variations of reflection coefficient, return loss and VSWR with inset distance for Antennas A, B and C

Antenna A				Antenna B				Antenna C			
y_0 (cm)	RC	VSWR	RL(dB)	y_0 (cm)	RC	VSWR	RL(dB)	y_0 (cm)	RC	VSWR	RL(dB)
0	0.7890	8.4800	2.0581	0	0.7736	7.8330	2.2299	0	0.7805	8.116	2.1526
0.0453	0.7538	7.1245	2.4545	0.1674	0.7367	6.5956	2.6543	0.1572	0.7471	6.9077	2.5326
0.0906	0.7012	5.6937	3.0830	0.3347	0.6782	5.2156	3.3725	0.3144	0.6932	5.5184	3.1831
0.1359	0.6246	4.3276	4.0880	0.5021	0.5857	3.8279	4.6459	0.4716	0.6063	4.0797	4.3466
0.1812	0.5192	3.1599	5.6930	0.6694	0.4395	2.5685	7.1401	0.6289	0.4641	2.7323	6.6670
0.2265	0.3948	2.3050	8.0714	0.8368	0.2189	1.5605	13.1944	0.7861	0.2332	1.6083	12.6446
0.2718	0.2974	1.8464	10.5341	1.0041	-0.0511	1.1077	25.8340	0.9433	-0.1003	1.2231	19.9707
0.3171	0.2931	1.8292	10.6597	1.1715	-0.2051	1.5161	13.7602	1.1005	-0.3912	2.2849	8.1529
0.3624	0.3856	2.2550	8.2780	1.3389	-0.0783	1.1699	22.1242	1.2577	-0.3284	1.9779	9.6723
0.4077	0.5101	3.0822	5.8475	1.5062	0.1900	1.4692	14.4241	1.4149	0.0073	1.0148	42.6841
0.4530	0.6176	4.2296	4.1864	1.6736	0.4191	2.4427	7.5544	1.5722	0.3140	1.9154	10.0616

CONCLUSION

The modelling and simulation of a rectangular microstrip antenna in MATLAB has been presented. Antennas are successfully modelled and simulated to operate at specified frequencies with specified dielectrics. Were modelled and simulated. For specified antenna parameters, appropriate dimensions of the patch antenna are obtained with the aid of transmission line model. Cavity model gives the radiation pattern analysis in form of the electric and magnetic field plots.

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